

***Preliminary Criticality Safety
Evaluation for In Situ Grouting
in the Subsurface Disposal
Area***

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Preliminary Criticality Safety Evaluation for In-Situ Grouting in the Subsurface Disposal Area

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Abstract

A preliminary criticality safety evaluation is presented for in situ grouting in the Subsurface Disposal Area (SDA) at the Idaho National Engineering Laboratory. The grouting materials evaluated are cement and paraffin.

The evaluation determines physical and administrative controls necessary to preclude criticality and identifies additional information required for a final criticality safety evaluation.

The evaluation shows that there are no criticality concerns with cementitious grout but a neutron poison such as boron would be required for the use of the paraffin matrix.

Key words: boron, cement, concrete, controls, criticality, fissile, grout, injection, in situ, keff, paraffin, plutonium, Rocky Flats, waste

List of Acronyms

CERCLA	Comprehensive Environmental Response, Compensation, and Liability Act
DOE	Department of Energy
EDF	Engineering Design File
EPA	Environmental Protection Agency
FS	feasibility study
IDHW	Idaho Department of Health and Welfare
INEEL	Idaho National Engineering & Environmental Laboratory
k_{eff}	effective multiplication
MCNP	Monte Carlo N-Particle Transport Code
ml	milliliter
OU	Operating Unit
PCSE	Preliminary Criticality Safety Evaluation
Pu	plutonium
RFP	Rocky Flats Plant
RI	remediation investigation
SDA	Subsurface Disposal Area
TRU	transuranic waste
WAG	waste area group

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1.0 Introduction

This document presents the preliminary criticality safety evaluation (PCSE) for in situ grouting (ISG) in the Subsurface Disposal Area (SDA) at the Idaho National Engineering and Environmental Laboratory (INEEL). The SDA is located within the Radioactive Waste Management Complex (RWMC). The SDA was used to dispose of radioactive waste material in underground pits, trenches, soil vault rows, and similar structures. The majority of the waste buried in the SDA consists of by-products from the Department of Energy (DOE) Rocky Flats Plant (RFP) nuclear weapons program plutonium manufacturing process. The remaining waste is from INEEL onsite disposal and non-RFP offsite disposal.

The current contingency project plan is to perform ISG treatability studies to support the Waste Area Group (WAG) 7-13/14 remediation investigation (RI) and feasibility study (FS) process. The plan is developed by the DOE-Idaho Operations Office, the Environmental Protection Agency (EPA) Region 10, and the Idaho Department of Health and Welfare (IDHW).

The purpose of this document is to assess the proposed plans in conjunction with the method of operation to identify criticality controls related to ISG to ensure that a criticality hazard is not likely under credible scenarios. This document is issued in support of the Preliminary Safety Analysis Report (PSAR).

2.0 Process Description

The primary objective of this treatability study is to address the remaining questions relative to the use of in situ grouting to stabilize the variety of heterogeneous wastes and intermixed soils found in the SDA. Data will be gathered to provide information for evaluation of Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA) criteria as part of the feasibility study for the WAG 7-13/14.

The stabilization concept includes injection of various cementitious, mineralogical, or polymeric stabilization agents into the void space created from the buried waste and contaminated soil matrix. Upon solidification, the resultant waste form encapsulates the buried waste material within a dense matrix, isolating the waste from surface and groundwater infiltration. Figure 1 illustrates a general view of the grouting operation. The reader is encouraged to become familiar with *In-Situ Buried Waste Stabilization Technologies at the Idaho National Engineering and Environmental Laboratory* (July 1998) for the details of the probing operation. The following sections describe the grouting operation in more detail and evaluate the criticality implications.

2.1 Waste Content

The precise content of the waste in the SDA is unknown. Several studies have been completed to estimate the contents of the waste disposed in the SDA (Thomas, and Clements). A more complete study is currently in progress to map the entire SDA and provide a graphical representation of the location of individual disposals and the contents of the shipments. Waste shipment log sheets have been discovered from the RFP that contain information such as the generator, amount of waste, and waste type. When the study is complete, generalizations can be made to determine the hazardous and radionuclide content of the waste. However, the exact fissile content of the waste will still be unknown. This is evident by the number of drums identified at the RWMC as overloaded. An Engineering Design File (EDF) by East (RWMC-EDF-800) identifies 13 overloaded drums that have been discovered to date at the RWMC. An overloaded drum is defined as containing more than 380 grams Pu-239 fissile gram equivalent

(FGE). This mass limit is based on 75% of the minimum critical handbook value of 510 grams (Paxton, Pruvost, 1987) for an optimally moderated plutonium system. Table 1 summarizes the 13 overloaded drums and indicates the waste code of the suspect overloaded drums and the fissile mass.

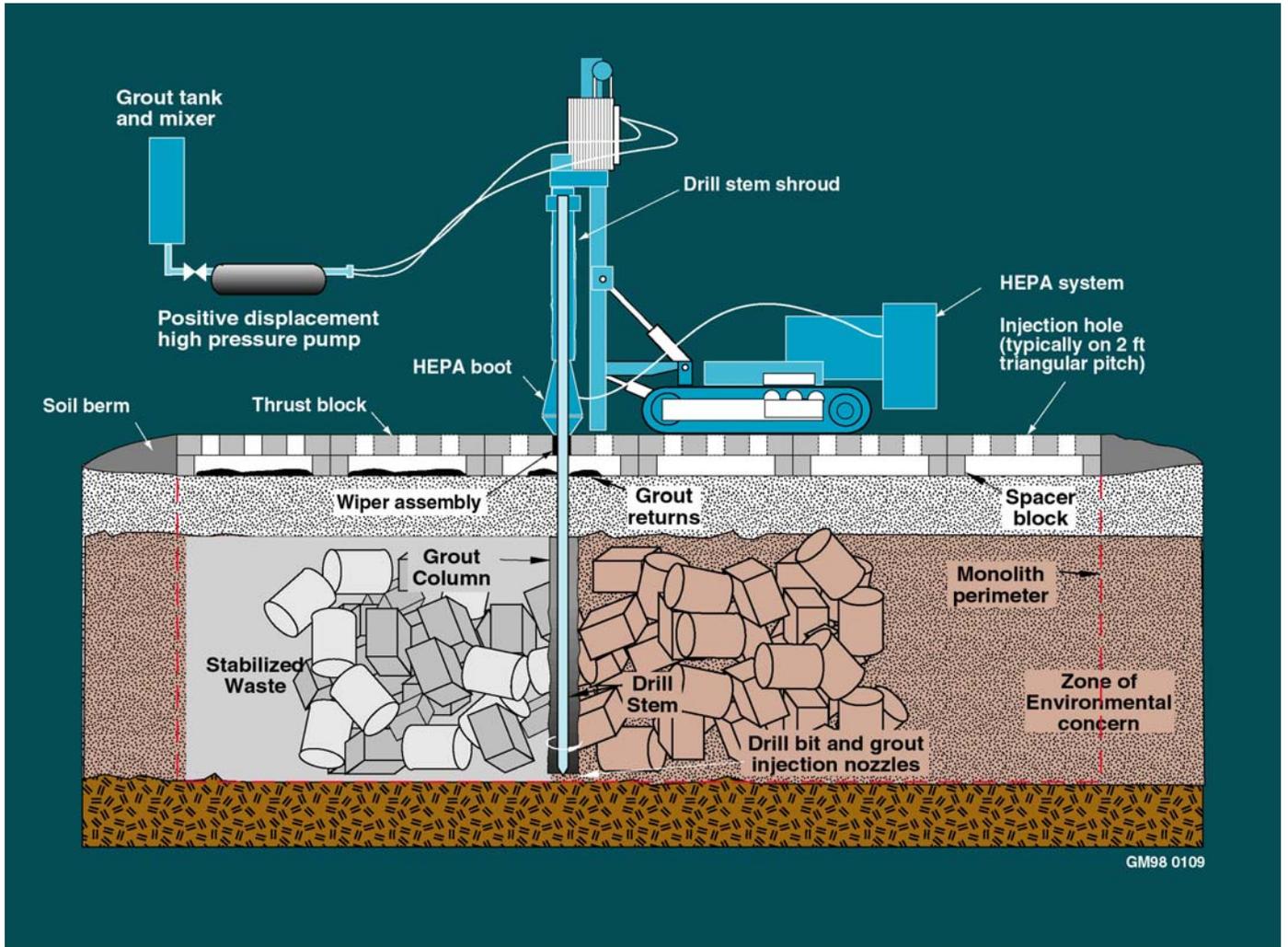


Figure 1. General Schematic of Grouting Operation.

Table 1. Summary of Overloaded Drums Identified at the RWMC

Waste Code	Maximum Measured Fissile Mass Plus Uncertainty (grams)
393	992
393	689
393	974
376	631
376	427
393	543
376	1,138
393	766
409	396
393	1,360
393	536
372	462
409	544

Table 1 indicates that one drum containing 1,360 grams of fissile mass has been identified to date at the RWMC. This mass can function as the bounding fissile mass starting point, but by no means is this the bounding fissile mass contained in the disposal area. A description of the content codes can be found in Table 2. Content code 409 was generated from September 1982 through January 1986, which corresponds to the time frame when the SDA was closed to underground disposal; therefore content code 409 is not disposed of in the SDA.

Table 2. Waste Code Description.

Waste Code	Content Description	Waste Description
372	Grit	Complete waste description is not available. Available information indicates the waste consists of "grit," such as aluminum oxide and iron fines or pellets, used in grit blasting operations.
376	Cemented Insulation and Filter Media	Pre-1979 wastes consist primarily of filter media removed from various filters (pre-filters, absolute filters, etc.). Since then, the waste consists of filter media and whole filters. Portland cement has been added to all waste packages. The Portland cement is added as a precautionary measure to neutralize any residual nitric acid that may be present in the waste and reduce the potential for drum pressurization.
393	Sand, Slag, and Crucible Heels	Waste consists of the insoluble residue of "heel" generated from processing magnesium oxide sand, slag, and magnesium oxide crucibles contaminated with above discard amounts of plutonium.
409	Molten Salt 30% Unpulverized	This waste consists of spent salt generated by the molten salt extraction process used to extract americium contamination from plutonium metal.

2.2 ISG Operations

The basic premise of the ISG technology is to inject grout material into a selected subsurface area (waste pit) and produce a stable monolith. The monolith provides for both hot spot retrieval with enhanced contamination control, and/or encapsulation and stabilization of buried waste for in situ disposal. A series of beneficial bench-scale material studies and associated field-scale implementation tests have been performed. In 1997 the technology was successfully tested in the acid pit located within WAG 7 13/14. For a complete description of the acid pit treatment, the readers are encouraged to familiarize themselves with the *Acid Pit Stabilization Project* (INEEL/EXT-98-00009). A general description of the ISG operation is discussed in the following subsections.

2.2.1 Treatment Technology Description

The grouting apparatus consists of a modified well drilling system as illustrated in Figure 1. The main components of the apparatus include a Casa Grande C-6 track mounted drilling/grouting rig or equivalent, drill stem, pump and hopper assembly, and thrust block. The drill stem is driven into the subsurface using rotopercussion powered by the Casa Grande C-6 or equivalent. The drill stem has a diameter of nine centimeters and a nozzle attached to the end. While the drill stem is being driven into the subsurface, a small flow of grouting material is released from the nozzle to reduce the friction. The drill stem is driven through the targeted contaminated

zone until the designated depth is reached (depth of waste). Once the drill stem has reached the designated depth, grouting material is injected at 400 bars (5,800 psi) through the rotating drill stem into the waste zone. The drill stem is withdrawn in precise increments to allow the grouting material to fill all of the available void space within the waste. The nominal drill stem withdrawal time is one to two minutes. The process is repeated, using a nominal 50 cm triangle pitch as illustrated in Figure 2, until a series of interconnected columns form a solid monolith within the waste matrix. A thrust block is used to maintain the spacing of grouting holes and to control the release of grouting material to the surface. The thrust block consists of a concrete block four feet wide, eight feet long, and eight to twelve inches thick. The thrust block contains five inch diameter holes drilled through the thickness in a triangle pattern to establish the grid pattern and act as starter holes. The thrust block is illustrated in Figure 2.

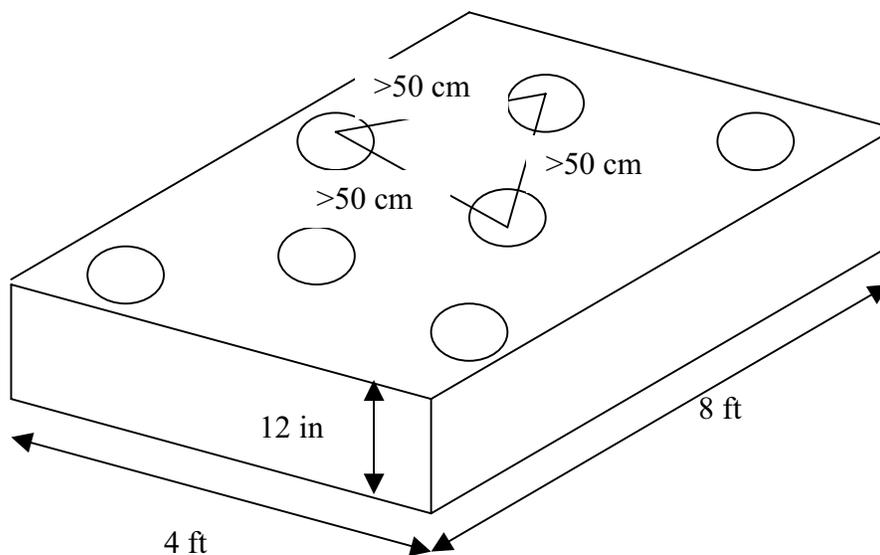


Figure 2. Top View of Thrust Block with Nominal Dimensions (Isometric)

2.2.2 Grouting Material

The two grouting materials proposed for this project include a Type-H (sulfate resistant) Portland cement grout and a paraffin grout. The cementitious grout is designed for block encapsulation of buried waste by the jet grouting process. The low viscosity grout (cement) is formulated to allow mixing and delivery in ordinary concrete trucks. The grout hardens on average of one day after injection when mixed with the soil. The paraffin grout is a low temperature natural paraffin wax based material originally developed for jet grouting leakage of hydrofluoric acid from surface impoundments. The additives within the molten paraffin allow the paraffin to blend with and even permeate soils regardless of their moisture content. The additives are multiple surfactants that also cause the grout to bond to water, oil, and buried debris. The paraffin grout is designed to fully encapsulate buried waste and to isolate the waste from water. Paraffin grouted areas will fill fractures and will minimize the potential of fugitive dust during excavation.

3.0 Requirements Documentation

This section specifies unique DOE orders or guides, ANS standards, Code of Federal Regulations, or internal requirement documents which apply to this CSE. General requirement documents such as DOE O 420.1, Section 4.3, ANSI/ANS 8.1, and PRD-112 (poison requirements) apply to all evaluations.

4.0 Methodology

The criticality analysis methodology uses the Monte Carlo N-Particle Transport Code (MCNP) System computer program to assess the criticality potential associated with the ISG treatability study. This section describes the MCNP program and the validation of the MCNP code.

4.1 Description of Method

MCNP is a general purpose code for calculating the time-dependent continuous-energy transport of neutrons, photons, and/or electrons in three-dimensional geometries. The MCNP code is used for many applications, such as nuclear criticality safety, radiation shielding, fission heating, and many other nuclear-related topics. The code is used in this application to determine k_{eff} and k_{∞} . The finite multiplication (k_{eff}) is a measure of a finite system's ability to sustain a nuclear chain reaction. The infinite multiplication (k_{∞}) is a measure of an infinite system's ability to sustain a nuclear chain reaction. A system is defined as critical if $k=1$, supercritical if $k>1$, or subcritical if $k<1$.

4.2 Validation

According to Whalen et al., *MCNP: Neutron Benchmark Problems*, "The general purpose Monte Carlo transport code MCNP has been tested on criticality, pulsed sphere, and shielding neutron problem families. Results for each were compared to experimental data. MCNP successfully predicted the experimental results of all three families within the expected data and statistical uncertainties. These successful predictions demonstrate that MCNP can successfully model a broad spectrum of neutron transport problems."

The MCNP program was performed on a Hewlett-Packard Series 9000 workstation using the HP-UNIX 10.20 operating system. MCNP-4b using the ENDF/B-V cross-section data was used to calculate the results. The MCNP-4b code on the workstations is verified per company software quality assurance plans (INEEL/INT-98-01140).

The results from this CSE are intended indicate the margin of safety and are not used to set fissile mass limits. The use of neutron absorbers and validation of the results will be addressed in the final CSE.

5.0 Discussion of Contingencies

The double contingency principle, required by the Department of Energy (DOE), states "The double contingency principle shall be used as a minimum to ensure that a criticality accident is an extremely unlikely event. Compliance with the double contingency principle requires that two unlikely, independent, and concurrent changes in process or system conditions occur before a criticality accident is possible." (DOE O 420.1)

For cementitious grouts consideration has been given to all credible scenarios within the ISG treatability study that could have an impact on criticality safety. There are adequate margins of safety within the nature of the cementitious operation to ensure that a criticality accident is not credible; although, the use of paraffin grouts will require additional controls. The margin of safety includes the inability of sufficient plutonium to accumulate in a favorable geometry with necessary moderation, reflection, and minimal diluent. If credit is taken for adding boron within the paraffin to reduce the moderation effects of paraffin, an adequate process must be in place to guarantee the boron remains in the paraffin at the designated concentration (that is, the boron does not leach out of the paraffin due to environmental and/or application effects). The margin of safety for this project is discussed in detail in the following section.

6.0 Evaluation and Results

6.1 Evaluation

Process knowledge and archived shipping reports indicate that the waste containers are in various stages of deterioration. The integrity of the containers may range from completely disintegrated to structurally sound. Therefore, the possibility of puncturing an overloaded drum and concentrating fissile material from the grouting operation does exist. The identified plutonium pathways resulting in the accumulation of plutonium are compaction of the waste and injecting the grout into the subsurface. A detailed discussion of each identified pathway is discussed in the following subsections.

6.1.1 Compaction

As the drill stem is inserted into the waste environment, the potential for the waste to become locally compacted or consolidated increases. The consolidation of the fissile mass may result in a small increase in the reactivity of the waste; however, the small diameter of the drill stem will limit the compaction/consolidation of the waste. The accumulation of fissile material within the drill stem is not of concern because the drill stem is geometrically safe (nine centimeter diameter). In addition, grouting matrix will be released from the drill stem at a positive flow while the drill stem is inserted into the subsurface.

6.1.2 Injection

The grouting matrix is ejected from the drill stem nozzle at a pressure of 400 bars and produces a nominal radial mixing distance of grouting matrix and waste of 29 centimeters. The drill stem is withdrawn in 5 centimeter increments and grouting matrix is injected into the waste media for approximately four to six seconds. The total nominal effected mixing volume is 13.2 liters. This volume equates to approximately 6% of a disposed drum. Therefore, there is minimal potential for plutonium migration/consolidation from injecting the grout into the subsurface.

6.2 Assessment

A preliminary criticality evaluation of the planned ISG treatability study assessing the criticality potential for the project has been completed to determine if a credible fissile mass can accumulate from the grouting activities. Calculations were conducted to determine a mass of plutonium to obtain a k_{∞} and k_{eff} of 1.00 for different grouting materials. The finite volume calculations simulated a 55-gallon drum and half of a 55-gallon drum. For conservatism, the drum volume was modeled as a sphere. The grouting materials include cementitious and paraffin products. Cementitious grouts are poor moderators whereas paraffin is an excellent moderator. Neutron poisons can be mixed with the paraffin to minimize moderation.

Although the fissile mass contained in the subsurface pit is unknown and cannot be accurately defined, grouting scenarios can be simulated to estimate the amount of fissile mass required for criticality. Once the amount of fissile mass to create criticality is estimated, engineering judgments can be made to determine if there is sufficient fissile mass within the subsurface for a credible event.

The following sections outline the methods of criticality control evaluated for the ISG treatability study and present the results from the analysis.

6.3 Computer Modeling Assumptions

Assumptions required to formulate the input models for the MCNP computer code include the fissile nuclide and grout matrix. For conservative purposes, Pu-239 was assumed as the fissile nuclide. Plutonium bounds U-235 that may be disposed within the SDA. Table 3 indicates the composition of cured grout. Several different elemental concrete grouts will be used to encapsulate the waste. Of the grouts investigated for this preliminary criticality safety evaluation, the elemental composition of the grout listed in this PCSE represents the most conservative (that is, the most reactive). This is primarily due to the low iron content. The final CSE will evaluate the grouts of choice; although it is not anticipated that there is a more reactive cementitious grout matrix. Table 4 indicates the composition of the paraffin grout (C₂₅H₅₂). The paraffin poison evaluated is Boron 10. The density of the cured concrete grout is 2.35 g/cm³. and the density of the paraffin grout is 0.93 g/cm³. The moisture content of the concrete grout was varied to determine the most reactive moisture content. The nominal moisture content for this type of application is 50 wt% although one type of cementitious grout that will be applied has a 33 wt% moisture content. The plutonium was assumed to be homogeneously dispersed throughout the grouting matrix.

Table 3. Composition of Concrete Grout.

Material	Mass Fraction
H	0.0056
O	0.4956
Si	0.3135
Al	0.0456
Na	0.0171
Ca	0.0826
Fe	0.0122
K	0.0192
Mg	0.0024
S	0.0012

Table 4. Compositions of Paraffin Grout.

Material	Mass Fraction
C	0.8514
H	0.1486

An infinite system of both grouting materials was modeled to achieve the most conservative plutonium concentration within the grouting matrix. In addition, spheres (208, and 104 liters) were also modeled to determine a finite plutonium concentration.

6.4 Results

Neutron multiplication factor k_{eff} and k_{∞} were calculated for the two grouting materials to determine the minimum concentration of plutonium to obtain a k-effective and k-infinity of 1.00. The finite arrays were modeled with 24 inches of reflection with the respective grouting medium (concrete or paraffin). The 24 inches of reflection represents a near infinite reflective system. The results of the computer calculations are given in Table 5 and Table 6. The calculations were generated to determine the mass of plutonium necessary for a criticality.

Table 5 represents the infinite and finite concrete matrix computer results. The first (Case Number) column indicates the MCNP input deck filename. The second (Water Percent) column provides the mass fraction of water. The third (Pu Density) column represents the critical plutonium concentration. The fourth (Finite Pu Mass) column designates the finite mass required for a criticality event (only given for the finite cases). The fifth (H/Pu) column indicates the hydrogen to plutonium ratio within the grouting matrix. The sixth ($k_{\text{inf}} \pm 2\sigma$) column lists the multiplication factor and two standard deviations.

Table 5. Concrete Matrix Results.

Concrete Matrix					
Infinite System					
Case #	Water Percent (wt %)	Pu Density (g/cm ³)		H/Pu (a%)	k _{inf} ± 2σ
Conc1	50	0.0063		3,092	0.9925 ± 0.0006
Conc	30	0.0052		2,850	0.9952 ± 0.0006
Conc2	10	0.0040		1,982	0.9923 ± 0.0008
Finite Volume 208 Liters (55-gallons)					
Case #	Water Percent (wt %)	Pu Density (g/ cm ³)	Finite Pu Mass (g)	H/Pu	k _{eff} ± 2σ
Drum1	50	0.0097	2,020	2,008	1.0005 ± 0.0016
Drum	30	0.0100	2,080	1,527	1.0019 ± 0.0020
Drum2	10	0.0118	2,450	672	1.0039 ± 0.0024
Finite Volume 104 Liters					
Case #	Water Percent (wt %)	Pu Density (g/ cm ³)	Finite Pu Mass (g)	H/Pu	k _{eff} ± 2σ
Drum11	50	0.0121	1,260	1,610	1.0003 ± 0.0020
Drum0	30	0.0131	1,360	1,131	1.0041 ± 0.0032
Drum22	10	0.0212	2,200	374	1.0033 ± 0.0028

The results from Table 5 indicate that an infinite system with cured grout (10% moisture content) is the most reactive. The most reactive finite volume is the moist grout (50% moisture content). In addition, the results indicate that a smaller volume (104 liters) requires less fissile mass for a critical system than a larger volume (55-gal). The plutonium mass required for a criticality in the smaller volume (104 liters) is 1,260 grams. Also, the results indicate that the plutonium concentration increases as the volume decreases; this is due to neutron leakage. Parametric studies for the concrete matrix infinite and finite systems can be found in Appendix C.

Table 6 represents the infinite and finite paraffin matrix computer results. The first (Case Number) column indicates the MCNP input deck filename. The second (Boron Percent) column provides the mass fraction of boron in the paraffin grout. The third (Pu Density) column represents the critical plutonium concentration. The fourth (H/Pu) column indicates the hydrogen to plutonium ratio within the grouting matrix. The fifth (Finite Pu Mass) column designates the finite mass required for a criticality event. The sixth (k_{inf} ± 2σ) column lists the multiplication factor and two standard deviations.

Table 6. Paraffin Matrix Results

Paraffin Matrix					
Infinite System					
Case #	Boron Percent (wt %)	Pu Density (g/ cm ³)		H/Pu (a%)	$k_{inf} \pm 2\sigma$
Paraffwo	N/A	0.0097		3,378	0.9998 ± 0.0006
Paraff1%	1.060E-04	0.0097		3,378	0.7406 ± 0.0010
Finite Volume 208 Liters					
Case #	Boron Percent (wt %)	Pu Density (g/ cm ³)	Finite Pu Mass (g)	H/Pu	$k_{eff} \pm 2\sigma$
Drum3	N/A	0.01125	2,340	2,913	0.9976 ± 0.0012
Drum4	1.062E-04	0.01125	2,340	2,913	0.7490 ± 0.0014
Finite Volume 104 Liters					
Case #	Boron Percent (wt %)	Pu Density (g/ cm ³)	Finite Pu Mass (g)	H/Pu	$k_{eff} \pm 2\sigma$
Drum33	N/A	0.0128	1,330	2,560	1.0005 ± 0.0016
Drum44	1.061E-04	0.0128	1,330	2,560	0.7692 ± 0.0016

The results from Table 6 indicate that the finite volume representing half of a nominal disposal drum volume (104 liters) is more reactive. The required plutonium mass to create a criticality for the smaller volume (104 liters) is 1,330 grams. The plutonium density increases as the volume decreases; this is due to neutron leakage. Parametric studies for the paraffin matrix infinite and finite systems can be found in Appendix C.

6.5 Discussion of Results

The results indicate a large quantity of homogeneously mixed plutonium in the grouting matrix is required to create a criticality event. The concrete moisture content was varied to represent the conditions that will be experienced within the SDA. The 50% moisture content represents the nominal moisture content at which the grout will be injected into the subsurface. The 30% moisture content represents one type of grout that will be used, and the 10% moisture content represents a cured grout. The computer modeling results for the finite scenario indicate that the 50% moisture content is the most reactive. The required unsafe mass of plutonium for a finite volume (104 liters) to create a criticality event is 1,260 grams.

Scenarios were also calculated for the paraffin grouts that will be used to encapsulate the buried waste. The required unsafe plutonium mass for the paraffin grout for a finite volume (104 liters) to create a criticality event is 1,330 grams. However, if boron (B-10) is added (0.0001 g/cc) within the paraffin, the plutonium mass to create a criticality event is greatly increased.

As the plutonium is dispersed homogeneously over the entire volume, of the drum, the system becomes overmoderated. There probably is no mechanism to homogeneously distribute the plutonium throughout the volume of a drum, the grout is most likely going to fill the voids within the waste contained in a drum. As the volume of the system is decreased, the mass of plutonium necessary to achieve a critical system decreases. This is due to the system shifting from an overmoderated system to an optimally moderated system. For plutonium paraffin

systems, the optimum H/Pu ratio occurs in the range of 500 to 700, depending upon the chosen reflector conditions. At these optimum moderation points, it should be noted that much less plutonium would be necessary to achieve a critical system: on the order of 400 to 500 grams. These optimally moderated systems are not likely to be achieved in the in-situ grouting process. Benchmark in-situ tests will indicate whether the paraffin will be dispersed evenly within the fissile material within "heterogeneous" areas of the waste matrix or the grouting process will tend to isolate these areas. The final CSE will address the results of the benchmark experiments and determine the realistic system for ISG stabilization. Finally, the scenarios assessed for this evaluation do not take credit for waste debris/diluent within the drums.

7.0 Design Features and Administratively Controlled Limits & Requirements

The following controls have been identified during this criticality safety evaluation. These controls are required to ensure criticality safety during probing operations in the SDA. Additional administrative and engineering controls may be identified for each probing campaign.

7.1 Grouting Operations

7.1.1 Administrative Controls

1. Preliminary calculations show that boron added to paraffin grouting matrix at a concentration of 1.00 g/l will have adequate criticality control.

7.1.2 Engineering Controls

At this time no engineering controls have been identified.

8.0 Summary & Conclusions

This preliminary criticality evaluation assesses the criticality potential of in situ grouting in the SDA. These analyses evaluate the criticality potential of injecting grout matrices into the SDA. Based on the analyses presented in this preliminary criticality safety evaluation, there are no criticality hazards from injecting cementitious grouting matrices within the SDA. The identified fissile mass with adequate moderation necessary for a criticality hazard, along with engineering and administrative controls identified by this evaluation, indicate that a criticality event will not occur under normal or postulated abnormal conditions.

Although this is a preliminary criticality safety evaluation, the data and results should not be viewed as preliminary. This evaluation is viewed as preliminary primarily based on the unknown results of plutonium migration (if any) from grout injection and whether the grouting materials can maintain boron concentrations at predetermined levels.

Finally, if boron is used as a poison, a process to measure boron concentration prior to insertion and an evaluation showing boron will remain homogeneously distributed within the paraffin under all environmental conditions is required.

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Appendix A

Table 7A. Concrete Atom Densities

Isotope or Element	Atoms/b-cm
Pu-239	2.4441-05
H	4.90088-02
O	3.6418-02
Si	4.7003-03
Al	7.1166-04
Na	3.1321-04
Ca	8.6781-04
Fe	9.1988-05
L	2.0678-04
Mg	4.580-05
S	1.5761-06

A plutonium concentration of 0.0097 was used to calculate the plutonium atom densities.

Table 8A. Paraffin Atom Densities

Isotope or Element	Atoms/b-cm
Pu-239	2.8346-05
C	3.9699-02
H	8.2571-02

Conc1

ISG CSE Plutonium Concentration in Concrete 50 wt% H2o

1 10 -1.4048 1 -2 -3 4 -5 6 \$ Pu Concrete matrix
2 0 (-1:2:3:-4:5:-6) \$ Outside World

- *1 pz 0
- *2 pz 100
- *3 px 50
- *4 px -50
- *5 py 50
- *6 py -50

mode n

imp:n 1 0

m10 94239.55c 1.5874-5 1001.50c 4.9088-2 8016.50c 3.6418-2
14000.50c 4.7003-3 13027.50c 7.1166-4 11023.50c 3.1321-4
20000.50c 8.6781-4 26000.55c 9.1988-5 19000.50c 6.9495-4
12000.50c 1.3974-4 16032.50c 5.2970-5

c

c

kcode 1000. 1.0 5 20

ksrc 10 10 10 20 20 20 30 30 30 40 40 40

-10 -10 10 -20 -20 20 -30 -30 30 -40 -40 40

10 10 30 20 20 30 30 30 30 40 40 30

-10 -10 30 -20 -20 30 -30 -30 30 -40 -40 30

c set time limit

c

ctme 9900

c

print

Conc

ISG CSE Plutonium Concentration in Concrete

1 10 -1.6722 1 -2 -3 4 -5 6 \$ Pu Concrete matrix
2 0 (-1:2:3:-4:5:-6) \$ Outside World

- *1 pz 0
- *2 pz 100
- *3 px 50
- *4 px -50
- *5 py 50
- *6 py -50

mode n

imp:n 1 0

m10 94239.55c 1.3102-5 1001.50c 3.7338-2 8016.50c 3.8484-2
14000.50c 7.8439-3 13027.50c 1.1876-3 11023.50c 5.2268-4
20000.50c 1.4482-3 26000.55c 1.5351-4 19000.50c 3.4508-4
12000.50c 6.9389-5 16032.50c 2.6302-5

c

c

kcode 1000. 1.0 15 400

ksrc 10 10 10 20 20 20 30 30 30 40 40 40

-10 -10 10 -20 -20 20 -30 -30 30 -40 -40 40

10 10 30 20 20 30 30 30 30 40 40 30

-10 -10 30 -20 -20 30 -30 -30 30 -40 -40 30

c set time limit

c

ctme 9900

c

print

Conc2

ISG CSE Plutonium Concentration in Concrete 10 wt% H2o

1 10 -2.0640 1 -2 -3 4 -5 6 \$ Pu Concrete matrix
2 0 (-1:2:3:-4:5:-6) \$ Outside World

- *1 pz 0
- *2 pz 100
- *3 px 50
- *4 px -50
- *5 py 50
- *6 py -50

mode n

imp:n 1 0

m10 94239.55c 1.0079-5 1001.50c 1.9975-2 8016.50c 4.1470-2
14000.50c 1.2463-2 13027.50c 1.8869-3 11023.50c 8.3045-4
20000.50c 2.3009-3 26000.55c 2.4390-4 19000.50c 5.4827-4
12000.50c 1.1025-4 16032.50c 4.1790-5

c

c

kcode 1000. 1.0 15 400

ksrc 10 10 10 20 20 20 30 30 30 40 40 40

-10 -10 10 -20 -20 20 -30 -30 30 -40 -40 40

10 10 30 20 20 30 30 30 30 40 40 30

-10 -10 30 -20 -20 30 -30 -30 30 -40 -40 30

c set time limit

c

ctme 9900

c

print

Drum1

ISG CSE 208 liter sphere Plutonium in Concrete reflected by concrete

1 10 -1.4082 -1 \$ Pu Concrete matrix
2 0 2 \$ Outside World
3 20 -1.3985 -2 1 \$ Concrete Reflection

1 s 0 0 0 36.8
2 s 0 0 0 100

mode n

imp:n 1 0 1

m10 94239.55c 2.4441-5 1001.50c 4.9088-2 8016.50c 3.6418-2
14000.50c 4.7003-3 13027.50c 7.1166-4 11023.50c 3.1321-4
20000.50c 8.6781-4 26000.55c 9.1988-5 19000.50c 2.0678-4
12000.50c 4.1580-5 16032.50c 1.5761-5
m20 1001.50c 4.9088-2 8016.50c 3.6418-2 14000.50c 4.7003-3
13027.50c 7.1166-4 11023.50c 3.1321-4 20000.50c 8.6781-4
26000.55c 9.1988-5 19000.50c 2.0678-4 12000.50c 4.1580-5
16032.50c 1.5761-5

c

c

kcode 1000. 1.0 15 400

ksrc 0 0 0 0 0 10 0 0 20 0 0 30 10 0 10 10 0 20 10 0 30 20 0 10
20 0 20 20 0 30 30 0 10 30 0 20 30 0 30 -10 0 10 -10 0 20
-10 0 30 -20 0 10 -20 0 20 -20 0 30 -30 0 10 -30 0 20 -30 0 30
0 0 -10 0 0 -20 0 0 -30 10 0 -10 10 0 -20 10 0 -30 20 0 -10
20 0 -20 20 0 -30 30 0 -10 30 0 -20 30 0 -30
-10 -10 30 -20 -20 30 -30 -30 30

c

c set time limit

c

ctme 9900

c

print

Drum

ISG CSE 208 liter sphere Plutonium in Concrete reflected by concrete

1 10 -1.6767 -1 \$ Pu Concrete matrix
2 0 2 \$ Outside World
3 20 -1.667 -2 1 \$ Concrete Reflection

1 s 0 0 0 36.8
2 s 0 0 0 100

mode n

imp:n 1 0 1

m10 94239.55c 2.4441-5 1001.50c 3.7338-2 8016.50c 3.8484-2
14000.50c 7.8439-3 13027.50c 1.1876-3 11023.50c 5.2268-4
20000.50c 1.4482-3 26000.55c 1.5351-4 19000.50c 3.4508-4
12000.50c 6.9389-5 16032.50c 2.6302-5
m20 1001.50c 3.7338-2 8016.50c 3.8484-2 14000.50c 7.8439-3
13027.50c 1.1876-3 11023.50c 5.2268-4 20000.50c 1.4482-3
26000.55c 1.5351-4 19000.50c 3.4508-4 12000.50c 6.9389-5
16032.50c 2.6302-5

c

c

kcode 1000. 1.0 15 400

ksrc 0 0 0 0 0 10 0 0 20 0 0 30 10 0 10 10 0 20 10 0 30 20 0 10
20 0 20 20 0 30 30 0 10 30 0 20 30 0 30 -10 0 10 -10 0 20
-10 0 30 -20 0 10 -20 0 20 -20 0 30 -30 0 10 -30 0 20 -30 0 30
0 0 -10 0 0 -20 0 0 -30 10 0 -10 10 0 -20 10 0 -30 20 0 -10
20 0 -20 20 0 -30 30 0 -10 30 0 -20 30 0 -30
-10 -10 30 -20 -20 30 -30 -30 30

c

c set time limit

c

ctme 9900

c

print

Drum2

ISG CSE 208 liter sphere Plutonium in Concrete reflected by concrete

1 10 -2.0718 -1 \$ Pu Concrete matrix
2 0 2 \$ Outside World
3 20 -2.06 -2 1 \$ Concrete Reflection

1 s 0 0 0 36.8
2 s 0 0 0 100

mode n

imp:n 1 0 1

m10 94239.55c 2.9732-5 1001.50c 1.9975-2 8016.50c 4.1470-2
14000.50c 1.2463-2 13027.50c 1.8869-3 11023.50c 8.3045-4
20000.50c 2.3009-3 26000.55c 2.4390-4 19000.50c 5.4827-4
12000.50c 1.1025-4 16032.50c 4.1790-5
m20 1001.50c 1.9975-2 8016.50c 4.1470-2 14000.50c 1.2463-2
13027.50c 1.8869-3 11023.50c 8.3045-4 20000.50c 2.3009-3
26000.55c 2.4390-4 19000.50c 5.4827-4 12000.50c 1.1025-4
16032.50c 4.1790-5

c

c

kcode 1000. 1.0 15 400

ksrc 0 0 0 0 0 10 0 0 20 0 0 30 10 0 10 10 0 20 10 0 30 20 0 10
20 0 20 20 0 30 30 0 10 30 0 20 30 0 30 -10 0 10 -10 0 20
-10 0 30 -20 0 10 -20 0 20 -20 0 30 -30 0 10 -30 0 20 -30 0 30
0 0 -10 0 0 -20 0 0 -30 10 0 -10 10 0 -20 10 0 -30 20 0 -10
20 0 -20 20 0 -30 30 0 -10 30 0 -20 30 0 -30
-10 -10 30 -20 -20 30 -30 -30 30

c

c set time limit

c

ctme 9900

c

print

Drum11

ISG CSE 208 liter sphere Plutonium in Concrete reflected by concrete

1 10 -1.4106 -1 \$ Pu Concrete matrix
2 0 2 \$ Outside World
3 20 -1.3985 -2 1 \$ Concrete Reflection

1 s 0 0 0 29.18
2 s 0 0 0 100

mode n

imp:n 1 0 1

m10 94239.55c 3.0488-5 1001.50c 4.9088-2 8016.50c 3.6418-2
14000.50c 4.7003-3 13027.50c 7.1166-4 11023.50c 3.1321-4
20000.50c 8.6781-4 26000.55c 9.1988-5 19000.50c 2.0678-4
12000.50c 4.1580-5 16032.50c 1.5761-5
m20 1001.50c 4.9088-2 8016.50c 3.6418-2 14000.50c 4.7003-3
13027.50c 7.1166-4 11023.50c 3.1321-4 20000.50c 8.6781-4
26000.55c 9.1988-5 19000.50c 2.0678-4 12000.50c 4.1580-5
16032.50c 1.5761-5

c

c

kcode 1000. 1.0 15 400

ksrc 0 0 0 0 0 10 0 0 20 0 0 30 10 0 10 10 0 20 10 0 30 20 0 10
20 0 20 20 0 30 30 0 10 30 0 20 30 0 30 -10 0 10 -10 0 20
-10 0 30 -20 0 10 -20 0 20 -20 0 30 -30 0 10 -30 0 20 -30 0 30
0 0 -10 0 0 -20 0 0 -30 10 0 -10 10 0 -20 10 0 -30 20 0 -10
20 0 -20 20 0 -30 30 0 -10 30 0 -20 30 0 -30
-10 -10 30 -20 -20 30 -30 -30 30

c

c set time limit

c

ctme 9900

c

print

Drum0

ISG CSE 208 liter sphere Plutonium in Concrete reflected by concrete

1 10 -1.6801 -1 \$ Pu Concrete matrix
2 0 2 \$ Outside World
3 20 -1.667 -2 1 \$ Concrete Reflection

1 s 0 0 0 29.18
2 s 0 0 0 100

mode n

imp:n 1 0 1

m10 94239.55c 3.3008-5 1001.50c 3.7338-2 8016.50c 3.8484-2
14000.50c 7.8439-3 13027.50c 1.1876-3 11023.50c 5.2268-4
20000.50c 1.4482-3 26000.55c 1.5351-4 19000.50c 3.4508-4
12000.50c 6.9389-5 16032.50c 2.6302-5
m20 1001.50c 3.7338-2 8016.50c 3.8484-2 14000.50c 7.8439-3
13027.50c 1.1876-3 11023.50c 5.2268-4 20000.50c 1.4482-3
26000.55c 1.5351-4 19000.50c 3.4508-4 12000.50c 6.9389-5
16032.50c 2.6302-5

c

c

kcode 1000. 1.0 15 400

ksrc 0 0 0 0 0 10 0 0 20 0 0 30 10 0 10 10 0 20 10 0 30 20 0 10
20 0 20 20 0 30 30 0 10 30 0 20 30 0 30 -10 0 10 -10 0 20
-10 0 30 -20 0 10 -20 0 20 -20 0 30 -30 0 10 -30 0 20 -30 0 30
0 0 -10 0 0 -20 0 0 -30 10 0 -10 10 0 -20 10 0 -30 20 0 -10
20 0 -20 20 0 -30 30 0 -10 30 0 -20 30 0 -30
-10 -10 30 -20 -20 30 -30 -30 30

c

c set time limit

c

ctme 9900

c

print

Drum22

ISG CSE 208 liter sphere Plutonium in Concrete reflected by concrete

1 10 -2.0812 -1 \$ Pu Concrete matrix
2 0 2 \$ Outside World
3 20 -2.06 -2 1 \$ Concrete Reflection

1 s 0 0 0 29.18
2 s 0 0 0 100

mode n

imp:n 1 0 1

m10 94239.55c 5.3417-5 1001.50c 1.9975-2 8016.50c 4.1470-2
14000.50c 1.2463-2 13027.50c 1.8869-3 11023.50c 8.3045-4
20000.50c 2.3009-3 26000.55c 2.4390-4 19000.50c 5.4827-4
12000.50c 1.1025-4 16032.50c 4.1790-5
m20 1001.50c 1.9975-2 8016.50c 4.1470-2 14000.50c 1.2463-2
13027.50c 1.8869-3 11023.50c 8.3045-4 20000.50c 2.3009-3
26000.55c 2.4390-4 19000.50c 5.4827-4 12000.50c 1.1025-4
16032.50c 4.1790-5

c

c

kcode 1000. 1.0 15 400

ksrc 0 0 0 0 0 10 0 0 20 0 0 30 10 0 10 10 0 20 10 0 30 20 0 10
20 0 20 20 0 30 30 0 10 30 0 20 30 0 30 -10 0 10 -10 0 20
-10 0 30 -20 0 10 -20 0 20 -20 0 30 -30 0 10 -30 0 20 -30 0 30
0 0 -10 0 0 -20 0 0 -30 10 0 -10 10 0 -20 10 0 -30 20 0 -10
20 0 -20 20 0 -30 30 0 -10 30 0 -20 30 0 -30
-10 -10 30 -20 -20 30 -30 -30 30

c

c set time limit

c

ctme 9900

c

print

Paraffwo

ISG CSE Plutonium Concentration in Paraffin Boron

1 10 -0.9397 1 -2 -3 4 -5 6 \$ Pu Paraffin matrix
2 0 (-1:2:3:-4:5:-6) \$ Outside World

- *1 pz 0
- *2 pz 100
- *3 px 50
- *4 px -50
- *5 py 50
- *6 py -50

mode n

imp:n 1 0

m10 94239.55c 2.4441-5 12000.50c 3.9699-2 1001.50c 8.2571-2

c

c

kcode 1000. 1.0 15 400

ksrc 10 10 10 20 20 20 30 30 30 40 40 40

-10 -10 10 -20 -20 20 -30 -30 30 -40 -40 40

10 10 30 20 20 30 30 30 30 40 40 30

-10 -10 30 -20 -20 30 -30 -30 30 -40 -40 30

c set time limit

c

ctme 9900

c

print

Paraff1%

ISG CSE Plutonium Concentration in Paraffin Boron

1 10 -.940 1 -2 -3 4 -5 6 \$ Pu Paraffin Boron matrix
2 0 (-1:2:3:-4:5:-6) \$ Outside World

- *1 pz 0
- *2 pz 100
- *3 px 50
- *4 px -50
- *5 py 50
- *6 py -50

mode n

imp:n 1 0

m10 94239.55c 2.4441-5 12000.50c 3.9699-2 1001.50c 8.2571-2
5010.50c 5.5708-6

c

c

kcode 1000. 1.0 15 400

ksrc 10 10 10 20 20 20 30 30 30 40 40 40

-10 -10 10 -20 -20 20 -30 -30 30 -40 -40 40

10 10 30 20 20 30 30 30 30 40 40 30

-10 -10 30 -20 -20 30 -30 -30 30 -40 -40 30

c set time limit

c

ctme 9900

c

print

Drum3

ISG CSE 208 liter sphere Plutonium in Paraffin reflected by Paraffin

1 10 -0.9413 -1 \$ Pu Paraffin matrix
2 0 2 \$ Outside World
3 20 -0.93 -2 1 \$ Paraffin Reflection

1 s 0 0 0 36.8
2 s 0 0 0 100

mode n

imp:n 1 0 1

m10 94239.55c 2.8346-5 6000.50c 3.9699-2 1001.50c 8.2571-2
m20 6000.50c 3.9699-2 1001.50c 8.2571-2

c

c

kcode 1000. 1.0 15 400

ksrc 0 0 0 0 0 10 0 0 20 0 0 30 10 0 10 10 0 20 10 0 30 20 0 10
20 0 20 20 0 30 30 0 10 30 0 20 30 0 30 -10 0 10 -10 0 20
-10 0 30 -20 0 10 -20 0 20 -20 0 30 -30 0 10 -30 0 20 -30 0 30
0 0 -10 0 0 -20 0 0 -30 10 0 -10 10 0 -20 10 0 -30 20 0 -10
20 0 -20 20 0 -30 30 0 -10 30 0 -20 30 0 -30
-10 -10 30 -20 -20 30 -30 -30 30

c

c set time limit

c

ctme 9900

c

print

Drum4

ISG CSE 208 liter sphere Plutonium in Paraffin reflected by Paraffin

1 10 -0.9414 -1 \$ Pu Paraffin matrix
2 0 2 \$ Outside World
3 20 -0.93 -2 1 \$ Paraffin Reflection

1 s 0 0 0 36.8
2 s 0 0 0 100

mode n

imp:n 1 0 1

m10 94239.55c 2.8346-5 6000.50c 3.9699-2 1001.50c 8.2571-2
5010.50c 5.5708-6
m20 6000.50c 3.9699-2 1001.50c 8.2571-2

c

c

kcode 1000. 1.0 15 400

ksrc 0 0 0 0 0 10 0 0 20 0 0 30 10 0 10 10 0 20 10 0 30 20 0 10
20 0 20 20 0 30 30 0 10 30 0 20 30 0 30 -10 0 10 -10 0 20
-10 0 30 -20 0 10 -20 0 20 -20 0 30 -30 0 10 -30 0 20 -30 0 30
0 0 -10 0 0 -20 0 0 -30 10 0 -10 10 0 -20 10 0 -30 20 0 -10
20 0 -20 20 0 -30 30 0 -10 30 0 -20 30 0 -30
-10 -10 30 -20 -20 30 -30 -30 30

c

c set time limit

c

ctme 9900

c

print

Drum33

ISG CSE 208 liter sphere Plutonium in Paraffin reflected by Paraffin

1 10 -0.9428 -1 \$ Pu Paraffin matrix
2 0 2 \$ Outside World
3 20 -0.93 -2 1 \$ Paraffin Reflection

1 s 0 0 0 29.18
2 s 0 0 0 100

mode n

imp:n 1 0 1

m10 94239.55c 3.2252-5 6000.50c 3.9699-2 1001.50c 8.2571-2
m20 6000.50c 3.9699-2 1001.50c 8.2571-2

c

c

kcode 1000. 1.0 15 400

ksrc 0 0 0 0 0 10 0 0 20 0 0 30 10 0 10 10 0 20 10 0 30 20 0 10
20 0 20 20 0 30 30 0 10 30 0 20 30 0 30 -10 0 10 -10 0 20
-10 0 30 -20 0 10 -20 0 20 -20 0 30 -30 0 10 -30 0 20 -30 0 30
0 0 -10 0 0 -20 0 0 -30 10 0 -10 10 0 -20 10 0 -30 20 0 -10
20 0 -20 20 0 -30 30 0 -10 30 0 -20 30 0 -30
-10 -10 30 -20 -20 30 -30 -30 30

c

c set time limit

c

ctme 9900

c

print

Drum44

ISG CSE 208 liter sphere Plutonium in Paraffin reflected by Paraffin

1 10 -0.9429 -1 \$ Pu Paraffin matrix
2 0 2 \$ Outside World
3 20 -0.93 -2 1 \$ Paraffin Reflection

1 s 0 0 0 29.18
2 s 0 0 0 100

mode n

imp:n 1 0 1

m10 94239.55c 3.2252-5 6000.50c 3.9699-2 1001.50c 8.2571-2
5010.50c 5.5708-6
m20 6000.50c 3.9699-2 1001.50c 8.2571-2

c

c

kcode 1000. 1.0 15 400

ksrc 0 0 0 0 0 10 0 0 20 0 0 30 10 0 10 10 0 20 10 0 30 20 0 10
20 0 20 20 0 30 30 0 10 30 0 20 30 0 30 -10 0 10 -10 0 20
-10 0 30 -20 0 10 -20 0 20 -20 0 30 -30 0 10 -30 0 20 -30 0 30
0 0 -10 0 0 -20 0 0 -30 10 0 -10 10 0 -20 10 0 -30 20 0 -10
20 0 -20 20 0 -30 30 0 -10 30 0 -20 30 0 -30
-10 -10 30 -20 -20 30 -30 -30 30

c

c set time limit

c

ctme 9900

c

print

Appendix C

Table 9C. Infinite Concrete Parametric Study

50 % Moisture Content	
Pu Concentration in Concrete (g/cc)	$k_{eff} \pm \sigma$
0.0083	1.1332 ± 0.0004
0.0073	1.0676 ± 0.0004
0.0063	0.9925 ± 0.0003
0.0053	0.9035 ± 0.0004
0.0043	0.7985 ± 0.0003
30% Moisture Content	
Pu Concentration in Concrete (g/cc)	$k_{eff} \pm \sigma$
0.0072	1.1609 ± 0.004
0.0062	1.0849 ± 0.004
0.0052	0.9952 ± 0.0003
0.0042	0.8855 ± 0.0003
0.0032	0.7510 ± 0.0003
10% Moisture Content	
Pu Concentration in Concrete (g/cc)	$k_{eff} \pm \sigma$
0.006	1.2109 ± 0.0004
0.005	1.1213 ± 0.0004
0.004	1.0041 ± 0.0004
0.003	0.8626 ± 0.0004
0.002	0.6691 ± 0.0003

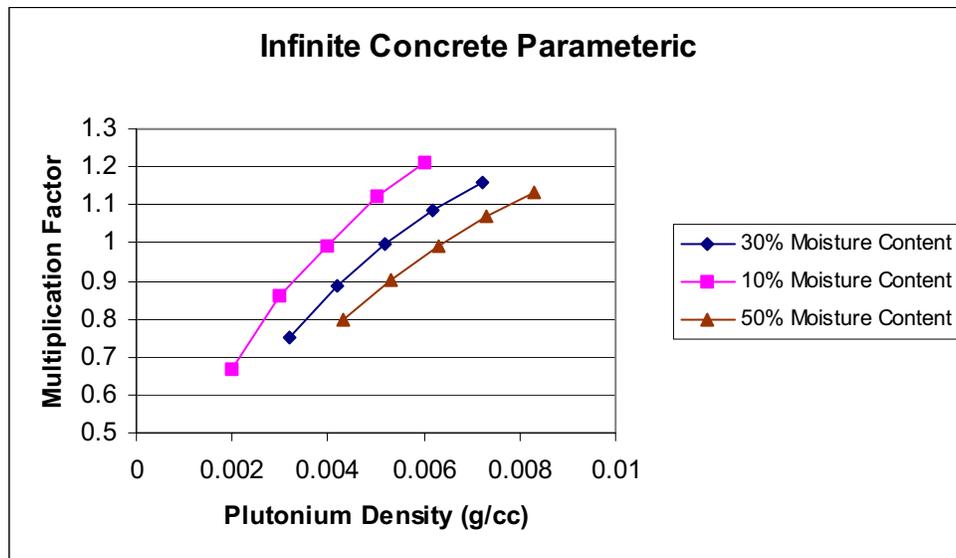


Figure 3C. Infinite Concrete Parametric Study.

Table 10C. Finite (208 Liter) Concrete Parameter Study.

50 % Moisture Content	
Pu Concentration in Concrete (g/cc)	$k_{eff} \pm \sigma$
0.0117	1.0779 ± 0.0009
0.0107	1.0437 ± 0.0009
0.0097	1.0005 ± 0.0009
0.0087	0.9535 ± 0.0008
0.0077	0.9014 ± 0.0008
30% Moisture Content	
Pu Concentration in Concrete (g/cc)	$k_{eff} \pm \sigma$
0.0117	1.0751 ± 0.0010
0.0107	1.0409 ± 0.0010
0.0097	1.0019 ± 0.0010
0.0087	0.9574 ± 0.0010
0.0077	0.9075 ± 0.0012
10% Moisture Content	
Pu Concentration in Concrete (g/cc)	$k_{eff} \pm \sigma$
0.0138	1.0480 ± 0.0013
0.128	1.0275 ± 0.0012
0.118	1.0039 ± 0.0012
0.0108	0.9746 ± 0.0011
0.0098	0.9437 ± 0.0012

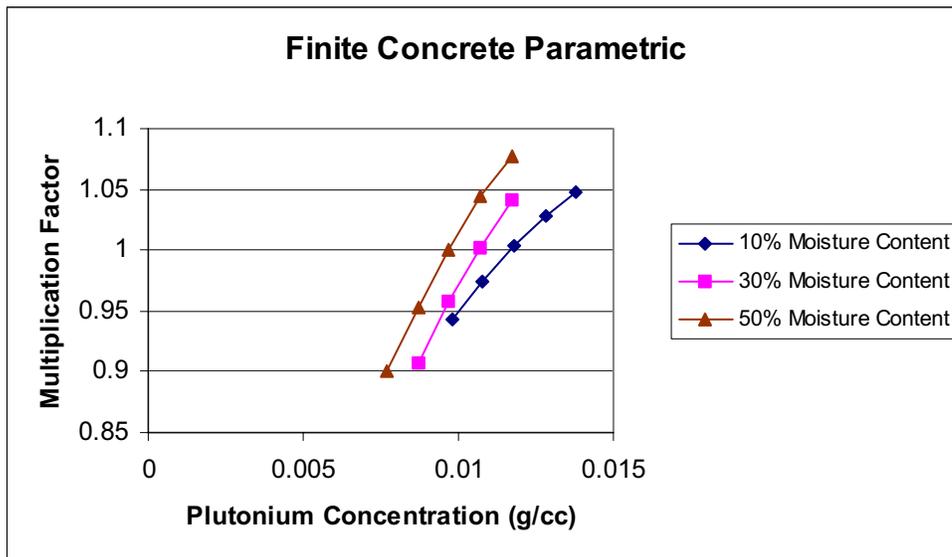


Figure 4C. Finite (208 Liter) Concrete Parametric Study.

Table 11C. Finite (104 Liter) Concrete Parametric Study.

50 % Moisture Content	
Pu Concentration in Concrete (g/cc)	$k_{eff} \pm \sigma$
0.0141	1.0579 ± 0.0010
0.0131	1.0273 ± 0.0011
0.0121	1.0003 ± 0.0010
0.0111	0.9641 ± 0.0010
0.0101	0.9281 ± 0.0009
30% Moisture Content	
Pu Concentration in Concrete (g/cc)	$k_{eff} \pm \sigma$
0.0151	1.0521 ± 0.0011
0.0141	1.0305 ± 0.0011
0.0131	1.0041 ± 0.0016
0.0121	0.9773 ± 0.0011
0.0111	0.9448 ± 0.0011
10% Moisture Content	
Pu Concentration in Concrete (g/cc)	$k_{eff} \pm \sigma$
0.0232	1.0206 ± 0.0013
0.0222	1.0135 ± 0.0013
0.0212	1.0033 ± 0.0014
0.0202	0.9964 ± 0.0013
0.0192	0.9843 ± 0.0013

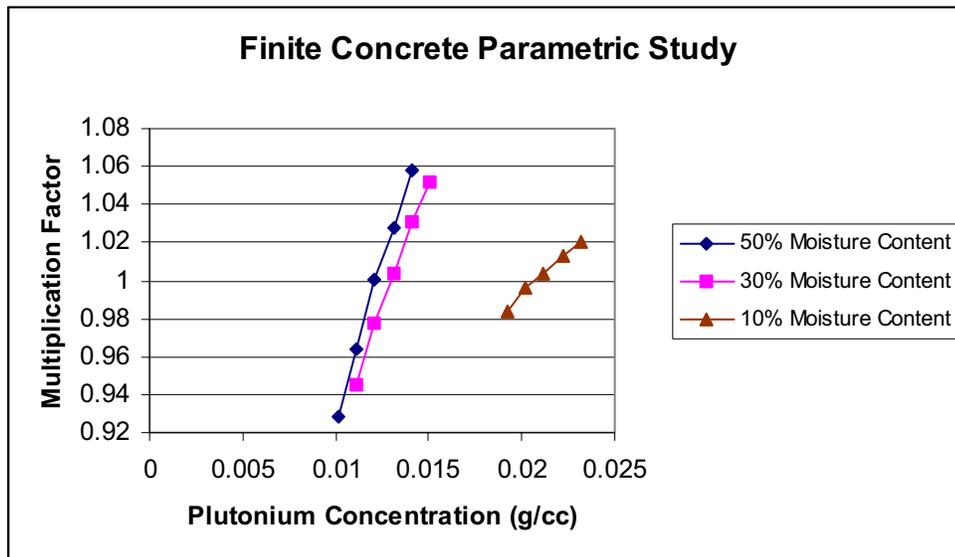


Figure 5C. Finite (104 Liter) Concrete Parametric Study.

Table 12C. Infinite Paraffin Parametric Study.

Paraffin Matrix	
Pu Concentration in Concrete (g/cc)	$k_{eff} \pm \sigma$
0.0117	1.0971 ± 0.0003
0.0107	1.0509 ± 0.0003
0.0097	0.9998 ± 0.0003
0.0087	0.9430 ± 0.0003
0.0077	0.8811 ± 0.0003

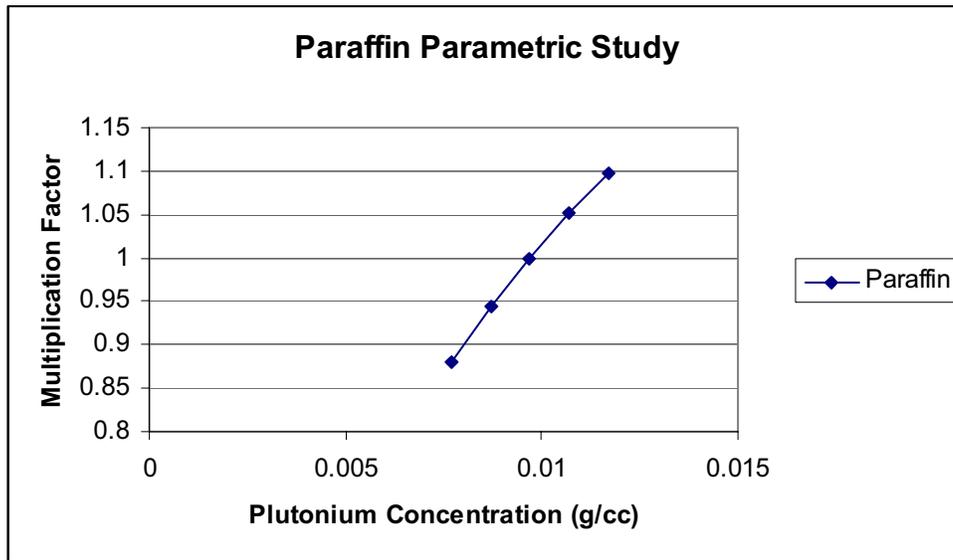


Figure 6C. Infinite Paraffin Parametric Study.

Table 13C. Finite (208 Liter)Paraffin Parametric Study.

Paraffin Matrix	
Pu Concentration in Concrete (g/cc)	$k_{eff} \pm \sigma$
0.01325	1.00719 ± 0.0007
0.01225	1.0355 ± 0.0007
0.01125	0.9976 ± 0.0006
0.01025	0.9525 ± 0.0007
0.00925	0.9025 ± 0.0007

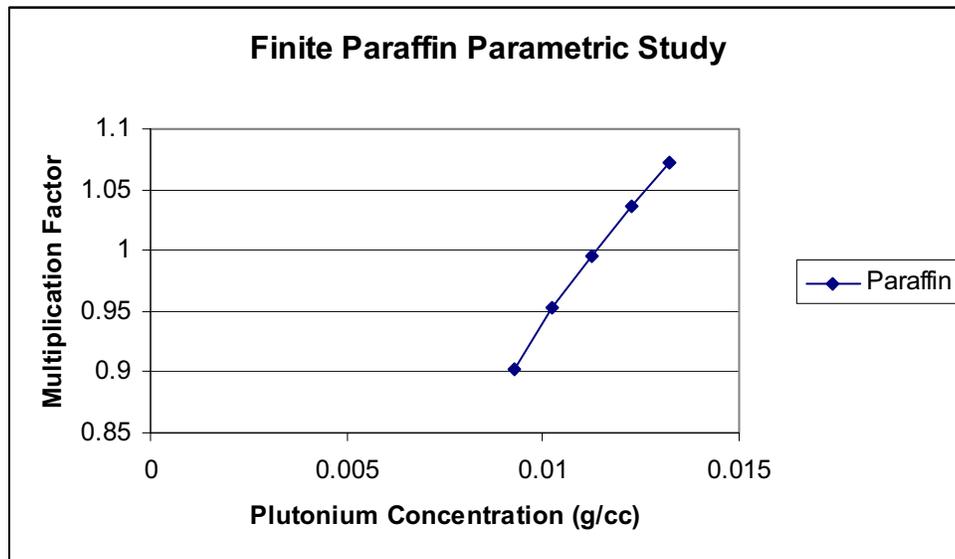


Figure 7C. Finite (208 Liter)Paraffin Parametric Study.

Table 14C. Finite (104 Liter) Paraffin Parametric Study.

Paraffin Matrix	
Pu Concentration in Concrete (g/cc)	$k_{eff} \pm \sigma$
0.0148	1.00648 ± 0.0008
0.0138	1.0334 ± 0.0008
0.0128	1.0005 ± 0.0008
0.0118	0.9635 ± 0.0008
0.0108	0.9213 ± 0.0007

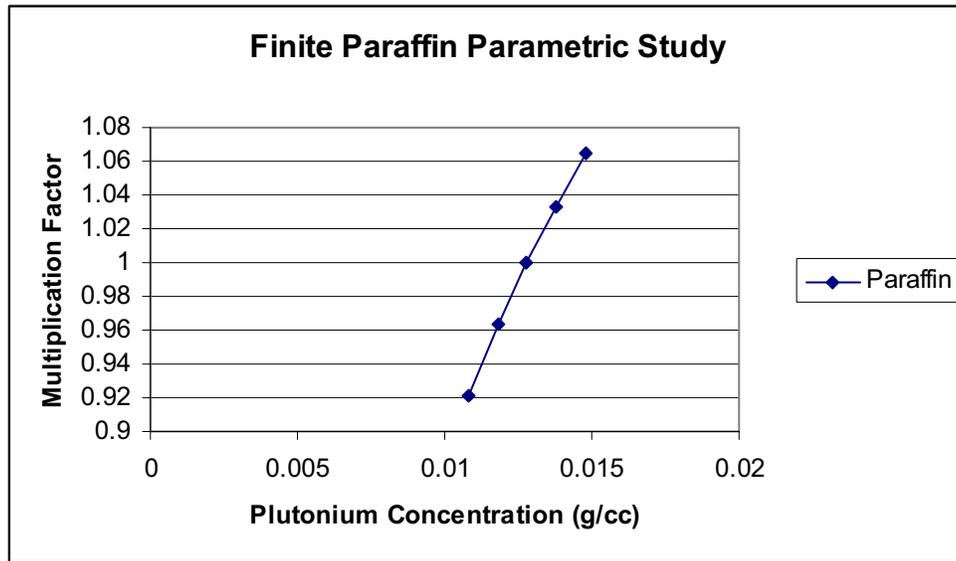


Figure 8C. Finite (104 Liter) Paraffin Parametric Study.